

DOIs:10.2019/JSHE/202302001

Research Paper / Article

Biocompatible Material Selection and Sensitivity Analysis for Femoral Component using Entropy based MCDM Methods: A Comparative Approach

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Abstract: In recent years, the world creating more and more global marketplaces, advanced technologies and efficient workers in medical sector. This global environment is forcing health organizations to accept almost everything into consideration at the same time. Increase flexibility is needed to remain competitive and respond to rapidly changing health sector. An effective material selection process is very important to the success of any operation. Biomaterials are used to perform the functions with living tissues in the body. Biomaterials are in contact with fluids continuously or for a certain period. The body's reactions are varying differently to these materials. Due to this, the proper biomaterial selection. To avoid the fatigue failure, a body system needs a suitable design considering mechanical properties. Due to the entropy process and sensitivity analysis, the results are more accurate as well as the design process is smooth. The methodology of Simple Additive Weighting (SAW), Multi Objective Optimization Ratio Analysis (MOORA), Technique for Order Preference by Similarity to Ideal Solution (TOPSIS) are implemented first time and comparative analysis is to determine the best material for better product development.

Key Words: Biocompatibility; Material Selection; MCDM; MOORA; SAW; TOPSIS; Orthopaedic; Health sector.

1. INTRODUCTION:

The femur bone [Fig:1] is also known as thigh bone. It is the longest and strongest bone in human body. It helps to stand and move in our body. This bone also supports important muscles, tendons, ligaments and circulatory system. It also helps to keep our balance. Femur bone only break from serious trauma like car accident, fall. Femur is also affected by osteoporosis.

If femur shaft fracture occurs, mainly surgical treatment needed. Sometimes very young children are treated with a cast. Mainly femur fractures are fixed within 24 to 48 hrs. two type of surgical procedure seen- external fixation and intra medullary nailing.

- External fixation: metal pins and screws are placed into the bone above and below the fracture site. Pins and screws are attached to bar outside the skin. This device holds the bones in the proper position. It is the temporary procedure for femur fracture.
- Intra medullary nailing: most surgeons used this method for treating femoral shaft fracture. In this procedure a specially designed metal road is inserted into the femur canal. Screws are placed above and below the fracture to hold the leg in correct alignment. these nails are usually made of titanium.





Fig:1: Femur Bone

This research ventures one of the major concerns in the field of strategy to select suitable material for femoral component of knee prosthesis based on a entropy method, namely SAW, MOORA, TOPSIS, in order to improve the longevity and quality of human life.

In this article, a novel MCDM methods have been used for orthopaedists/practitioners, and prosthesis and implant manufacturers. This project addresses modelling an automated selection methodology for orthopaedic research.

2. LITERATURE REVIEW :

In this section, the material selection methodologies are reviewed for replacing the existing material to select a right candidate material of Femoral component system of health sector, the selection of material methodologies presented in this article contains important selection attributes and its applications

- ✓ Bahraminasab M, Sahari B, Edwards K, Farahmand F, Jahan A, Hong T S and Arumugam M (2014): work on the influence of shape and material used for the femoral component pegs in knee prostheses for reducing the problem of aseptic loosening.
- ✓ Kabir G and Lizu A (2016) proposed that material selection for femoral component of total knee replacement integrating fuzzy AHP with PROMETHEE.
- ✓ Bahraminasab M and Jahan A (2011) researched on Material selection for femoral component of total knee replacement using comprehensive VIKOR.
- ✓ MEHMET ALPER SOFUOG[~] LU (2020) proposed on A new biomaterial selection approach using reference ideal method

3. METHODOLOGY :

3.1 Multi Criteria Decision Making (MCDM)

Considering multiple conflicting criteria, selecting the best path from a set of feasible alternatives known as Multiple criteria decision making (MCDM). This process always goes through at least two alternatives and two conflicting criteria. MCDM are divided two broad categories: Multiple Attribute Decision Making (MADM) and Multiple Objective Decision Making (MODM). Several useful tools for solving of MCDM problems are

- Simple Additive Weighting method (SAW)
- > Technique for Order Preference by Similarity to Ideal Solution (TOPSIS)
- Multi Objective Optimization Ratio Analysis (MOORA)
- Analytical Hierarchy Method (AHP)
- Analytical Network Method ANP etc.

3.2 Entropy Method

Entropy was originally a thermodynamic concept, first introduced into information theory by Shannon. It has been widely used in the engineering, socioeconomic and other fields. According to the basic principles of information theory, information is a measure of system's ordered degree, and the entropy is a measure of system's disorder degree [Table 2].

3.3 Sensitivity Analysis

In actual situation decision-making is rather dynamic not static process. Changing with environment it varies in the continuously. In reality the value of decision-making attitude depends upon decision maker's personal choice but



now a days the artificial intelligence remove the personal biases. Keeping it in mind, the proposed model for the selection of femur material has been enhanced by sensitivity analysis [Fig:4,6] to provide a readymade solution of the current problem under variable decision-making attitude[Table:6,12]. The governing equation of the material measure (AM) is given by

$$AM_i = \alpha (OFM_i - SFM_i) + SFM_i$$

where, i = 1, 2...m.

- OFM_i = Objective factor measure for the alternative i
- SFM_i = Subjective factor measure for the alternative i
- α = Objective factor decision weight/Coefficient of attitude

3.4 The Flowchart of the Proposed Methods



Fig: 2 Flowchart of Methodology

4. MATERIAL:

The selection of femoral component for total knee replacement in health sector considering technical, economic and supply aspects. The paper involves identification of different material [Table:1] that are used in the manufacturing of bio-material and to give a best result. Ten materials with five important properties are considered. The decision maker has to compare all the materials regarding each aspect and has to judge the best one, and this is difficult decision-making problem. So, these MCDM methods is applied to select optimal material in this section.

	C1	C2	C3	C4	C5
	Tensile	Elongation	Corrosion	Wear	Osseointegration
	strength		resistance	resistance	
	(MPa)				
M1	896	20	0.745	0.865	0.665
Co–Cr alloys (wrought Co–Ni–Cr–Mo)					
M2	655	20	0.745	0.865	0.665
Co–Cr alloys (castable Co–Cr–Mo)					
M3	1240	12	0.955	0.955	0.5
NiTi SMA					
M4	1000	12	0.745	0.955	0.955
Porous NiTi SMA					
M5	550	54	0.955	0.59	0.745
Ti alloys (pure Ti)					
M6	985	12	0.955	0.665	0.745



Ti6Al4V					
M7		12	0.665	0.745	0.59
SS L316 (cold worked)	862				
M8	517	40	0.665	0.59	0.59
SS L316 (annealed)					
M9	900	10	0.955	0.665	0.745
Ti-6Al-7Nb (IMI-367 wrought)					
M10	1050	12.5	0.955	0.665	0.745
Ti-6Al-7Nb (Protasul-100 hot forged)					

Table 1: Femur component material selection matrix [8]

5. RESEARCH GAP:

Selection and proper decision making brings success in any operation. When a problem arise for total knee replacement then proper decision approach is needed for human body system. Maximum biomaterial industry is spent their money to developed an efficient decision-making system. This paper is projected to improve this system in normal and emergency environment. According to literature review, biomaterial selection of femoral component in medical industry some piecemeal work has been done. Comparative analysis by various MCDM methods on Material selection process and Sensitivity analysis are implemented first to know the best material as well as the value of closeness.

6. PROBLEM FORMULATION :

In medical sector, biomaterials are made of stainless Steel and other materials. Among these five criteria [C]- Tensile strength, Corrosion resistance, Wear resistance and Osseointegration are beneficiary and rest of criteria are non-beneficiary. Find out the optimum result among alternatives[M] are difficult task. In the matter of total knee replacement, the proper material selection is challenging task to a decision maker. This paper involved to find out the best result among the alternatives considering criteria.

7. EXPERIMENT AND RESULT:

7.1 The weighted values from entropy method

	C1 Tensile strength (MPa)	C2 Elongation	C3 Corrosion resistance	C4 Wear resistance	C5 Osseointegration
weighted values	0.2247	0.0844	0.2667	0.1628	0.2614

Table 2:

7.2 In the SAW method

The weighted values got from entropy method STEP1: Determination of normalized decision matrix

Material	C1	C2	C3	C4	C5				
	Tensile	Elongation	Corrosion	Wear	Osseointegration				
	strength		resistance	resistance					
	(MPa)								
M1		0.3704	0.7801	0.9058	0.7519				
Co-Cr alloys (wrought Co-Ni-Cr-	0.7226								
Мо)									
M2	0.5282	0.3704	0.7801	0.9058	0.7519				
Co-Cr alloys (castable Co-Cr-Mo)									
M3		0.2222	1.0000	1.0000	1.0000				
NiTi SMA	1.0000								



M4		0.2222	0.7801	1.0000	0.5236
Porous NiTi SMA	0.8065				
M5	0.4435	1.0000	1.0000	0.6178	0.6711
Ti alloys (pure Ti)					
M6		0.2222	1.0000	0.6963	0.6711
Ti6Al4V	0.7944				
M7		0.2222	0.6963	0.7801	0.8475
SS L316 (cold worked)	0.6952				
M8	0.4169	0.7407	0.6963	0.6178	0.8475
SS L316 (annealed)					
M9	0.7258	0.1852	1.0000	0.6963	0.6711
Ti-6Al-7Nb (IMI-367 wrought)					
M10		0.2315	1.0000	0.6963	0.6711
Ti–6Al–7Nb (Protasul-100 hot	0.8468				
forged)					

Table 3:

STEP 2: Determination of weighted normalized decision matrix

Material	C1	C2	C3	C4	C5
	Tensile	Elongation	Corrosion	Wear	Osseointegration
	strength		resistance	resistance	
	(MPa)				
M1		0.0313	0.2080	0.1474	0.1965
Co-Cr alloys (wrought Co-Ni-	0.1624				
Cr-Mo)					
M2		0.0313	0.2080	0.1474	0.1965
Co-Cr alloys (castable Co-Cr-	0.1187				
Mo)					
M3		0.0188	0.2667	0.1628	0.2614
NiTi SMA	0.2247				
M4		0.0188	0.2080	0.1628	0.1369
Porous NiTi SMA	0.1812				
M5	0.0997	0.0844	0.2667	0.1006	0.1754
Ti alloys (pure Ti)					
M6		0.0188	0.2667	0.1134	0.1754
Ti6Al4V	0.1785				
M7		0.0188	0.1857	0.1270	0.2215
SS L316 (cold worked)	0.1562				
M8		0.0625	0.1857	0.1006	0.2215
SS L316 (annealed)	0.0937				
M9		0.0156	0.2667	0.1134	0.1754
Ti-6Al-7Nb (IMI-367 wrought)	0.1631				
M10		0.0195	0.2667	0.1134	0.1754
Ti–6Al–7Nb (Protasul-100 hot	0.1903				
forged)					

Table 4:

STEP 3: Computation of composite score s.....by sum of all weighted normalized rows The values of (s) are:



Material	M1 Co-Cr alloys (wrought Co-Ni- Cr-Mo)	M2 Co-Cr alloys (castable Co-Cr- Mo)	M3 NiTi SMA	M4 Porous NiTi SMA	M5 Ti alloys (pure Ti)	M6 Ti6Al4V	M7 SS L316 (cold worked)	M8 SS L316 (annealed)	M9 Ti–6Al– 7Nb (IMI-367 wrought)	M10 Ti–6Al– 7Nb (Protasul- 100 hot forged)
	0.7457	0.7020	0.9343	0.7077	0.7268	0.7527	0.7092	0.6640	0.7342	0.7653

Table 5:

STEP 4:





7.2.1 Sensitivity Analysis:

The value of closeness co-efficient in SAW method

Material	when	when
	alpha=0	alpha=1
M1	0.1965	0.5491
M2	0.1965	0.5054
M3	0.2614	0.6729
M4	0.1369	0.5708
M5	0.1754	0.5513
M6	0.1754	0.5773
M7	0.2215	0.4876
M8	0.2215	0.4425
M9	0.1754	0.5587
M10	0.1754	0.5898

Table 6:





Fig:4

7.3 In the MOORA method

The weig	hted values got from entropy method
STEP 1	Determination of normalized decision matrix

Material	C1	C2	C3	C4	C5
	Tensile	Elongation	Corrosion	Wear	Osseointegration
	strength		resistance	resistance	
	(MPa)				
M1		0.2551	0.2794	0.3562	0.2985
Co-Cr alloys (wrought Co-Ni-	0.3175				
Cr-Mo)					
M2		0.2551	0.2794	0.3562	0.2985
Co-Cr alloys (castable Co-Cr-	0.2321				
Mo)					
M3	0.4394	0.1530	0.3582	0.3932	0.2244
NiTi SMA					
M4		0.1530	0.2794	0.3932	0.4287
Porous NiTi SMA	0.3543				
M5		0.6887	0.3582	0.2429	0.3344
Ti alloys (pure Ti)	0.1949				
M6	0.3490	0.1530	0.3582	0.2738	0.3344
Ti6Al4V					
M7		0.1530	0.2494	0.3068	0.2648
SS L316 (cold worked)	0.3054				
M8		0.5101	0.2494	0.2429	0.2648
SS L316 (annealed)	0.1832				
M9		0.1275	0.3582	0.2738	0.3344
Ti-6Al-7Nb (IMI-367	0.3189				
wrought)					
M10		0.1594	0.3582	0.2738	0.3344
Ti–6Al–7Nb (Protasul-100 hot	0.3720				
forged)					



STEP 2: Determination of weighted normalized decision matrix

Material	C1	C2	C3	C4	C5
	Tensile	Elongation	Corrosion	Wear	Osseointegration
	strength		resistance	resistance	
	(MPa)				
M1		0.0215	0.0745	0.0580	0.0780
Co-Cr alloys (wrought Co-Ni-	0.0713				
Cr-Mo)					
M2		0.0215	0.0745	0.0580	0.0780
Co-Cr alloys (castable Co-Cr-	0.0522				
Mo)					
M3		0.0129	0.0955	0.0640	0.0587
NiTi SMA	0.0987				
M4		0.0129	0.0745	0.0640	0.1121
Porous NiTi SMA	0.0796				
M5	0.0438	0.0581	0.0955	0.0395	0.0874
Ti alloys (pure Ti)					
M6		0.0129	0.0955	0.0446	0.0874
Ti6Al4V	0.0784				
M7		0.0129	0.0665	0.0499	0.0692
SS L316 (cold worked)	0.0686				
M8	0.0412	0.0431	0.0665	0.0395	0.0692
SS L316 (annealed)					
M9		0.0108	0.0955	0.0446	0.0874
Ti-6Al-7Nb (IMI-367 wrought)	0.0717				
M10		0.0135	0.0955	0.0446	0.0874
Ti-6Al-7Nb (Protasul-100 hot	0.0836				
forged)					

Table 8

STEP 3: Determination of weighted multi objective optimization the value of asum of all weighted normalized values for all beneficial column

Material	M1	M2	M3	M4	M5					M10
	Co–Cr	Co–Cr	NiTi	Porous	Ti	M6	M7	M8	M9	Ti–6Al–
	alloys	alloys	SMA	NiTi	alloys	Ti6Al4V	SS L316	SS L316	Ti-6Al-	7Nb
	(wrought	(castable		SMA	(pure		(cold	(annealed)	7Nb	(Protasul-
	Co-Ni-	Co-Cr-			Ti)		worked)		(IMI-367	100 hot
	Cr-Mo)	Mo)							wrought)	forged)
	0.2254	0.2062	0.2712	0.2311	0.2370	0.2314	0.1980	0.1903	0.2225	0.2371

 Table 9:

the value of bsum of all weighted normalized values for all non-beneficial column

Material	M1 Co-Cr alloys (wrought Co-Ni- Cr-Mo)	M2 Co-Cr alloys (castable Co-Cr- Mo)	M3 NiTi SMA	M4 Porous NiTi SMA	M5 Ti alloys (pure Ti)	M6 Ti6Al4V	M7 SS L316 (cold worked)	M8 SS L316 (annealed)	M9 Ti-6Al- 7Nb (IMI-367 wrought)	M10 Ti–6Al– 7Nb (Protasul- 100 hot forged)
	0.0780	0.0780	0.0587	0.1121	0.0874	0.0874	0.0692	0.0692	0.0874	0.0874



STFP 4.	the value of a-h
SILL 4.	the value of a-0

Material	M1	M2	M3	M4	M5					M10
	Co-Cr	Co–Cr	NiTi	Porous	Ti	M6	M7	M8	M9	Ti–6Al–
	alloys	alloys	SMA	NiTi	alloys	Ti6Al4V	SS L316	SS L316	Ti–6Al–	7Nb
	(wrought	(castable		SMA	(pure		(cold	(annealed)	7Nb	(Protasul-
	Co-Ni-	Co-Cr-			Ti)		worked)		(IMI-367	100 hot
	Cr-Mo)	Mo)							wrought)	forged)
	0.1473	0.1281	0.2125	0.1190	0.1496	0.1440	0.1288	0.1211	0.1351	0.1497

STEP 5:

M4

Arranging the final value in descending order: ----->>> $M_3 > M_{10} > M_5 > M_{10} > M_{10} > M_5 > M_{10} >$



Fig:5

7.3.1 Sensitivity Analysis:

The value of closeness co-efficient in MOORA method

Material	when alpha=0	when alpha=1
M1	-0.0780	0.2254
M2	-0.0780	0.2062
M3	-0.0587	0.2712
M4	-0.1121	0.2311
M5	-0.0874	0.2370
M6	-0.0874	0.2314
M7	-0.0692	0.1980
M8	-0.0692	0.1903
M9	-0.0874	0.2225
M10	-0.0874	0.2371

Table 12:





Table 11:

M3 > M10 > M5 > M1 > M6 > M9 > M7 > M2 > M8 >



7.4 In the TOPSIS method

The weighted values got from entropy method

STEP1: Determination of normalized decision matrix

Material	C1	C2	C3	C4	C5
	Tensile	Elongation	Corrosion	Wear	Osseointegration
	strength		resistance	resistance	
	(MPa)				
M1		0.3704	0.7801	0.9058	0.7519
Co-Cr alloys (wrought Co-Ni-	0.7226				
Cr-Mo)					
M2		0.3704	0.7801	0.9058	0.7519
Co-Cr alloys (castable Co-Cr-	0.5282				
Mo)					
M3		0.2222	1.0000	1.0000	1.0000
NiTi SMA	1.0000				
M4		0.2222	0.7801	1.0000	0.5236
Porous NiTi SMA	0.8065				
M5	0.4435	1.0000	1.0000	0.6178	0.6711
Ti alloys (pure Ti)					
M6	0.7944	0.2222	1.0000	0.6963	0.6711
Ti6Al4V					
M7		0.2222	0.6963	0.7801	0.8475
SS L316 (cold worked)	0.6952				
M8		0.7407	0.6963	0.6178	0.8475
SS L316 (annealed)	0.4169				
M9	0.7258	0.1852	1.0000	0.6963	0.6711
Ti-6Al-7Nb (IMI-367 wrought)					
M10		0.2315	1.0000	0.6963	0.6711
Ti–6Al–7Nb (Protasul-100 hot	0.8468				
forged)					
		Table 13:			

STEP 2:

Determination of positive ideal solution: taking the maximum values of each column from the normalized decision matrix

Criteria	C1 Tensile strength (MPa)	C2 Elongation	C3 Corrosion resistance	C4 Wear resistance	C5 Osseointegration
	1	1	1	1	1

Table 14:

Determination of negative ideal solution: taking the minimum values of each column from the normalized decision matrix

Criteria	C1	C2	C3	C4	C5
	Tensile strength (MPa)	Elongation	Corrosion resistance	Wear resistance	Osseointegration
	0.4169	0.1852	0.6963	0.6178	0.5236

Table 15:



STEP 3:

Calculation of the separation measure from the positive ideal solution(di_Plus)

Material	M1 Co-Cr alloys (wrought Co-Ni- Cr-Mo)	M2 Co-Cr alloys (castable Co-Cr- Mo)	M3 NiTi SMA	M4 Porous NiTi SMA	M5 Ti alloys (pure Ti)	M6 Ti6Al4V	M7 SS L316 (cold worked)	M8 SS L316 (annealed)	M9 Ti–6Al– 7Nb (IMI-367 wrought)	M10 Ti-6Al- 7Nb (Protasul- 100 hot forged)
	0.2850	0.3375	0.2260	0.3629	0.3488	0.3223	0.3324	0.3695	0.3409	0.3137

Calculation of the seperation measure from the negetive ideal solution(di_Minus)

Material	M1 Co-Cr alloys (wrought Co-Ni- Cr-Mo)	M2 Co-Cr alloys (castable Co-Cr- Mo)	M3 NiTi SMA	M4 Porous NiTi SMA	M5 Ti alloys (pure Ti)	M6 Ti6Al4V	M7 SS L316 (cold worked)	M8 SS L316 (annealed)	M9 Ti-6Al- 7Nb (IMI-367 wrought)	M10 Ti-6Al- 7Nb (Protasul- 100 hot forged)
	0.2300	0.1862	0.4292	0.2447	0.2941	0.2518	0.2219	0.2313	0.2296	0.2702

Table 17:

STEP 3: Calculation of R_i

Material	M1 Co-Cr alloys (wrought Co-Ni- Cr-Mo)	M2 Co-Cr alloys (castable Co-Cr- Mo)	M3 NiTi SMA	M4 Porous NiTi SMA	M5 Ti alloys (pure Ti)	M6 Ti6Al4V	M7 SS L316 (cold worked)	M8 SS L316 (annealed)	M9 Ti–6Al– 7Nb (IMI-367 wrought)	M10 Ti-6Al- 7Nb (Protasul- 100 hot forged)
	0.4466	0.3556	0.6551	0.4027	0.4575	0.4386	0.4003	0.3850	0.4025	0.4627

Table 18:

STEP 4:

 $\label{eq:main_stars} Arranging the final value in descending order: ----->>> \qquad M3 > M10 > M5 > M1 > M6 > M4 > M9 > M7 > M8 > M2$





7.5 Comparative Analysis of MCDM Methods:

MATERIAL	SAW	MOORA	TOPSIS
	(RANK)	(RANK)	(RANK)
<mark>(M1)</mark>	4	4	4
(M2)	9	8	10
(M3)	1	1	1
(M4)	8	10	6
(M5)	6	3	3
(M6)	3	5	5
(M7)	7	7	8
(M8)	10	9	9
(M9)	5	6	7
(M10)	2	2	2

Table 19

8. **DISCUSSION**:

From the result, we see that for the three different processes of MCDM, the result is same. The ranking of first two choices is same for those different processes. In SAW, MOORA and TOPSIS methods, ranks of alternatives are given in descending order of their respective composite score. So, the ranking of alternatives of materials are as follows: NiTi SMA(M3) > Ti–6Al–7Nb (M10) It means that Material 3 and Material 10 are the best as it maximizes the benefit criteria respectively.

We have also made the sensitivity analysis with graphical representation in which we see that in SAW and MOORA methods. From the sensitivity analysis graph, we also get the rank of the lathes for any alpha value by drawing a vertical line from that alpha value to the straight line of the lathe in the graph. That's why for doing the sensitivity analysis our result does not depends any different decision makers with their different weighted values.

9. CONCLUSIONS :

It is quite clear that the use of SAW, MOORA and TOPSIS methods are observed to be quite capable and computationally easy to evaluate and select the proper femoral component from a given set of alternatives. These methods use the measures of the considered criteria with their relative importance in order to arrive at the final ranking of the alternative material. Thus, these popular MCDM methods can be successfully employed for solving knee replacement biomaterial selection decision-making problems having any number of criteria and alternatives in the manufacturing domain.

As a future scope, a fuzzy TOPSIS, fuzzy SAW, fuzzy MOORA based methodology may be developed to aid the decision makers to take decisions in health sector. The proposed future research work is planned into different stages: Objective setup, analysis of parameter and design of experiments, experimentation and validation of results, alternative solution search. In second phase the project research can be taken to the next level by designing in CATIA and finding the stress analysis by ANSYS and implementation of Finite Element Analysis (FEA) and henceforth comparing the life cycles. Application of software like Delcam would convert this theoretical approach to the final product, which in turn, would be of great help in medical sector.

DECLARATION BY AUTHORS

Ethical Approval: Approved Acknowledgement: None Source of Funding: None Conflict of Interest: The authors declare no conflict of interest.



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